

Does size really matter?

Rethinking monopile installation

Words: Fabian Hippe, Strategic & Commercial Director at Menck

As monopiles become larger and installation conditions more challenging, successful foundation installation depends on more than hammer capacity. Driveability, energy transfer, soil uncertainty, acoustic performance and live monitoring are all becoming critical to installing larger foundations safely, efficiently and with greater certainty.

Before a next-generation monopile is suspended above the seabed, most of the decisions that will determine whether it is installed successfully have already been made. The foundation has been designed, the hammer selected, the vessel mobilised and the driving plan approved. The soil, however, has not agreed to any of it.

That is where the next step-up in offshore wind foundation size becomes difficult. Piles are becoming larger in diameter, longer and heavier, but the uncertainty beneath them remains. As foundations increase in size, relatively small deviations between predicted and actual soil behaviour can have significant consequences. What appears to be a minor variation in a model can lead to pile run, premature refusal, excessive fatigue and costly vessel downtime.

The answer is not simply a larger hammer. More available energy and greater installation capability are essential, but successful installation depends on how effectively that energy is transferred into the pile, how quickly the pile's response can be understood and how effectively the operation can adapt while driving is still under way.

Experience from today's large-monopile campaigns is already shaping the equipment, monitoring and control systems required for future foundations. The next generation must combine greater capacity with precision: purpose-designed installation technology, sufficient operational flexibility, acoustic performance considered from the outset and digital insight capable of turning every blow into a better informed decision.

The industry has proved it can build bigger. The real test is whether it can install bigger with even greater certainty.

Installation must shape foundation design

Foundation design has traditionally focused heavily on the in-place condition: structural loads, fatigue life and steel quantity. Those considerations remain essential, but they cannot be separated from installability.

As piles increase in diameter, length and weight, projects need to evaluate the practical installation envelope much earlier. This includes hammer capacity, pile-top geometry, lifting constraints, vessel capability, expected penetration behaviour, fatigue consumption and the consequences of events such as pile run or premature refusal.

Preinstallation driveability analyses and Soil Resistance to Driving (SRD) models therefore remain indispensable. They establish the expected relationship between hammer capability, pile behaviour and soil resistance and provide the basis for hammer selection and the driving strategy. But they remain predictions.

They are built on assumptions about soil layering, stiffness, damping, cyclic response characteristics and energy transfer. Offshore soils rarely follow a perfectly uniform model, and the larger the foundation and installation spread become, the more costly a deviation from those assumptions can be.

The strongest projects therefore use predictions to shape the installation strategy rather than treating them as a guarantee. They consider the preferred driving method, operating limits, decision gates and contingency routes before mobilisation. In difficult ground conditions, this could include relief drilling or a drilled-and-grouted solution planned from the outset to support successful installation.

This is about optimising the complete project rather than a single component. A foundation that uses slightly more steel but can be installed reliably may ultimately create more value than a highly optimised design that introduces disproportionate installation risk.

More power is not the best answer

Larger monopiles require greater installation capability. A hammer needs sufficient ram mass to provide the required energy to progress the pile through the expected soil profile while maintaining acceptable penetration rates. However, maximum rated energy alone does not define performance.

Every impact creates a dynamic interaction between the hammer, pile and soil in which the pile is embedded. Part of the delivered energy contributes to permanent pile penetration, while part is absorbed through soil damping, pile deformation, rebound and other dynamic effects. Performance therefore depends not simply on the amount of energy released, but on how that energy travels through the complete impact chain and into the foundation.

The ram, anvil, hammer and pile adaptation serving as the interface to the pile all influence the force-time signature at the pile head. Ram mass and impact velocity are particularly important. The same theoretical impact energy can be generated through different combinations of mass and velocity, but the resulting interaction with the pile is not necessarily the same.

The next generation of pile installation will therefore depend on more than energy alone. What matters is how efficiently that energy is transferred, how clearly the pile response can be observed and how quickly the operation can act on that information.



The next generation of hammer technology cannot simply be a larger version of equipment developed for smaller foundations. It must be designed around future offshore wind operating conditions.

This thinking has shaped the development of Menck's Windhammer, the MHU 6000W. The hammer is designed to deliver up to 6,250 kJ and accommodate monopiles with top diameters of up to nine metres. Those figures provide the required capacity, but equally important is how that capacity is generated and controlled.

The Windhammer uses a heavier ram and purpose-designed impact chain to deliver high impact energy through a longer and smoother force-time profile. Rather than pursuing the sharpest possible strike, the objective is to produce a longer, more controlled force profile while transferring the required energy into the pile efficiently.

That distinction becomes more important as pile dimensions increase. High energy must be delivered without unnecessarily increasing peak loads within the pile or impact chain, while sufficient momentum must be maintained to achieve effective penetration.

Operational flexibility is equally important. Even within the same wind farm, individual foundations can encounter different soil conditions. Hammer capability therefore needs to cover an operating range rather than a single design point. The ability to adjust energy, stroke and blow rate allows installation teams to respond to the behaviour being observed while maintaining established controls on hammer and pile performance.

Where required, additional hydraulic boosting can provide further contingency against challenging localised soil resistance without changing the selected hammer configuration. Such capability should complement rather than replace appropriate hammer selection:



Fabian Hippe

the hammer should be capable of meeting the anticipated driving conditions under its normal operating parameters, with boosting providing additional flexibility when required.

Installation and acoustic performance work together

The way energy is delivered also affects acoustic performance. Rapid deformation of a steel pile during impact is a major source of underwater noise. The force-time signature generated at the pile head therefore influences not only penetration performance and structural response, but also the acoustic signature of the installation.

By influencing the duration and shape of the applied force, it is possible to affect that acoustic response while maintaining the energy and momentum required for penetration.

Noise mitigation can therefore no longer be treated only as an external system added after the hammer and pile have been selected. It increasingly needs to be considered within hammer design, the impact chain and the overall installation methodology.

The MHU 6000W can also be configured with source-based noise mitigation, allowing the driving and acoustic strategies to be considered together rather than as separate project requirements.

From predicted performance to live control

Purpose-designed hardware is only one part of preparing for larger piles. As pile dimensions increase, the industry also needs a better understanding of what is happening during every blow.

High-frequency monitoring can provide a live view of hammer behaviour, pile response, penetration per blow, energy transfer and force-time signatures at the pile head. The significance is not the volume of data collected, but the speed with which it can support a useful operational decision.

Before driving begins, engineers have a predicted installation profile. Once driving starts, the pile begins producing evidence of how the actual system is behaving.

The ability to compare the two is increasingly important.

When actual behaviour begins to diverge from the predicted profile, operators can see the change as it develops. Hammer energy and blow rate can be adjusted within the approved operating envelope to manage penetration, fatigue and noise footprint. Energy delivery can be optimised for the soil response being observed. Developing pile-run conditions can be recognised earlier, while unexpected increases in resistance can be assessed before they develop into a refusal event.

This does not remove uncertainty; it allows the operation to respond to uncertainty earlier. It turns monitoring from a post-installation record into an operational control tool.

A smart hammer is not simply a hammer fitted with more sensors. It is part of an integrated installation system that captures the quality of each impact, relates measured pile behaviour to engineering expectations and presents that information in time to support the next operational decision. The value lies in the link between measurement, interpretation and action.

Our newest hammer is being developed within that environment. Its capacity is designed for the next generation of larger monopiles, while its monitoring and control capabilities are intended to make that capacity visible and manageable. At 6,250 kJ, knowing that the energy has been released is not enough. The project also needs to understand how effectively it has been transferred, how the pile has responded and whether the operation remains within the expected installation envelope.

Today, digital monitoring can bring measured performance and engineering interpretation closer to the point of decision. The longer-term direction is towards increasingly closed-loop installation control, where advanced analytics help teams adapt operating parameters as measured conditions evolve.

Operator judgement and established control procedures will remain central. The opportunity is to provide those operators and engineers with better information, earlier, so that intervention takes place before a developing condition becomes an installation problem.

Building a learning installation system

Monitoring also creates value beyond the pile currently being driven. Each installation records the relationship between hammer settings, soil response, pile behaviour and achieved penetration. That information can improve the next pile in the campaign and refine driveability models, equipment selection and foundation design for future projects.

Operational experience illustrates the potential. On one offshore campaign, eight jacket piles experienced a pile run. Lessons from that work were carried into a later wind farm in the same area as the previous installation, involving more than 300 piles, where digital insight into equipment performance and pile response supported a different operational approach. No pile-run events were recorded. The value was in converting operational experience into better preparation, earlier recognition and more informed control.

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This creates an ongoing link between engineering and execution. Predictions guide the initial plan. Live measurements show where reality differs. Operational decisions respond, and the resulting data improves the next prediction in real time.

For developers and installation contractors, better control can reduce exposure to pile run and refusal, support more efficient use of hammer capacity, manage fatigue consumption, limit unnecessary equipment wear and improve schedule predictability.

With high-value installation vessels operating on the project's critical path, even modest improvements in installation efficiency and predictability can have a significant impact across an entire campaign.

Looking at the whole installation system

The transition to larger monopiles is not solely an equipment challenge; it is a system challenge.

Hammer design, foundation geometry, geotechnical interpretation, acoustic performance, vessel integration, fatigue management, contingency methods and operational data all need to point towards the same outcome.

Optimising them independently can create interfaces and transfer risk from one package to another. Considering them together provides a more realistic view of installability, operational risk and whole-project cost.

The sector will continue to demand larger and more capable equipment, but capability

should not be confused with uncontrolled force. Preparing for the next generation means involving installation expertise earlier, designing energy delivery and acoustic performance together, providing sufficient operational flexibility and putting digital systems in place to learn from every blow.

The next generation of offshore wind will be built on larger foundations. Its success will depend on applying greater capability with greater intelligence, evidence and control. Bigger foundations will require bigger equipment, but installing them successfully will depend on much more than size alone.

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